

Engineering System Solutions

Building Relationships | Exceeding Expectations

Structural

Mechanical

Electrical

Plumbing

Commissioning

3632 North Rancho Drive Las Vegas, Nevada 89130 4943 North 29th East, Suite A Idaho Falls, Idaho 83401 1677 Eureka Road, Suite 102 Roseville, California 95661

STRUCTURAL CALCULATIONS

FOF

City of Las Vegas Dept. of Public Works

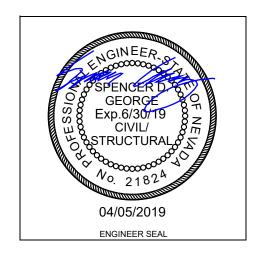
Fremont Street Light Pole Foundations

Las Vegas, NV

ES² Project #: 19.2010 April 5, 2019

SHEET INDEX

Basis For Design	S
Foundation Design	S





Basis For Design

ATC Hazards by Location

Search Information

Address: Fremont St, Las Vegas, NV, USA

Coordinates: 36.1619681, -115.12373530000002

Elevation: 1888 ft

Timestamp: 2019-03-08T17:29:23.579Z

Hazard Type: Wind



ASCE 7-16	ASCE 7-10	ASCE 7-05
MRI 10-Year 70 mph	MRI 10-Year 76 mph	ASCE 7-05 Wind Speed 90 mph
MRI 25-Year 75 mph	MRI 25-Year84 mph	
MRI 50-Year 80 mph	MRI 50-Year 90 mph	
MRI 100-Year 85 mph	MRI 100-Year 96 mph	
Risk Category I	Risk Category I 105 mph	
Risk Category II 99 mph	Risk Category II 115 mph	
Risk Category III 105 mph	Risk Category III-IV 120 mph	
Risk Category IV 110 mph		

The results indicated here DO NOT reflect any state or local amendments to the values or any delineation lines made during the building code adoption process. Users should confirm any output obtained from this tool with the local Authority Having Jurisdiction before proceeding with design.

Disclaimer

Hazard loads are interpolated from data provided in ASCE 7 and rounded up to the nearest whole integer. Per ASCE 7, islands and coastal areas outside the last contour should use the last wind speed contour of the coastal area – in some cases, this website will extrapolate past the last wind speed contour and therefore, provide a wind speed that is slightly higher. NOTE: For queries near wind-borne debris region boundaries, the resulting determination is sensitive to rounding which may affect whether or not it is considered to be within a wind-borne debris region.

Mountainous terrain, gorges, ocean promontories, and special wind regions shall be examined for unusual wind conditions.

While the information presented on this website is believed to be correct, ATC and its sponsors and contributors assume no responsibility or liability for its accuracy. The material presented in the report should not be used or relied upon for any specific application without competent examination and verification of its accuracy, suitability and applicability by engineers or other licensed professionals. ATC does not intend that the use of this information replace the sound judgment of such competent professionals, having experience and knowledge in the field of practice, nor to substitute for the standard of care required of such professionals in interpreting and applying the results of the report provided by this website. Users of the information from this website assume all liability arising from such use. Use of the output of this website does not imply approval by the governing building code bodies responsible for building code approval and interpretation for the building site described by latitude/longitude location in the report.

ATC Hazards by Location

Search Information

Address: Fremont St, Las Vegas, NV, USA

Coordinates: 36.1619681, -115.12373530000002

Elevation: 1888 ft

Timestamp: 2019-03-08T17:30:58.480Z

Hazard Type: Seismic

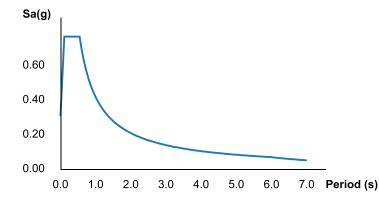
Reference ASCE7-16

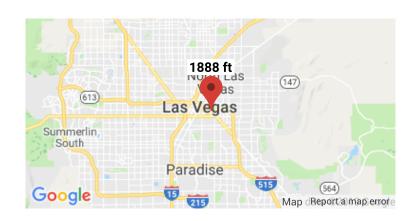
Document:

Risk Category:

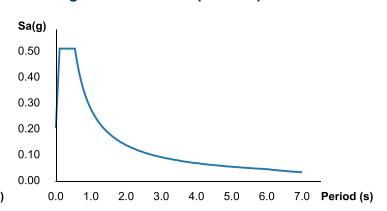
Site Class: D-default

MCER Horizontal Response Spectrum





Design Horizontal Response Spectrum



Basic Parameters

Name	Value	Description
S _S	0.572	MCE _R ground motion (period=0.2s)
S ₁	0.188	MCE _R ground motion (period=1.0s)
S _{MS}	0.768	Site-modified spectral acceleration value
S _{M1}	0.418	Site-modified spectral acceleration value
S _{DS}	0.512	Numeric seismic design value at 0.2s SA
S _{D1}	0.278	Numeric seismic design value at 1.0s SA

▼Additional Information

Name	Value	Description
SDC	D	Seismic design category
Fa	1.343	Site amplification factor at 0.2s
F _v	2.225	Site amplification factor at 1.0s
	0.897	Coefficient of risk (0.2s)

CR _S		
CR ₁	0.919	Coefficient of risk (1.0s)
PGA	0.251	MCE _G peak ground acceleration
F _{PGA}	1.349	Site amplification factor at PGA
PGA _M	0.339	Site modified peak ground acceleration
TL	6	Long-period transition period (s)
SsRT	0.572	Probabilistic risk-targeted ground motion (0.2s)
SsUH	0.638	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
SsD	1.764	Factored deterministic acceleration value (0.2s)
S1RT	0.188	Probabilistic risk-targeted ground motion (1.0s)
S1UH	0.204	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
S1D	0.6	Factored deterministic acceleration value (1.0s)
PGAd	0.696	Factored deterministic acceleration value (PGA)

The results indicated here DO NOT reflect any state or local amendments to the values or any delineation lines made during the building code adoption process. Users should confirm any output obtained from this tool with the local Authority Having Jurisdiction before proceeding with design.

Disclaimer

Hazard loads are provided by the U.S. Geological Survey Seismic Design Web Services.

While the information presented on this website is believed to be correct, ATC and its sponsors and contributors assume no responsibility or liability for its accuracy. The material presented in the report should not be used or relied upon for any specific application without competent examination and verification of its accuracy, suitability and applicability by engineers or other licensed professionals. ATC does not intend that the use of this information replace the sound judgment of such competent professionals, having experience and knowledge in the field of practice, nor to substitute for the standard of care required of such professionals in interpreting and applying the results of the report provided by this website. Users of the information from this website assume all liability arising from such use. Use of the output of this website does not imply approval by the governing building code bodies responsible for building code approval and interpretation for the building site described by latitude/longitude location in the report.



Structural Design

NOTES: Delphi Pole

DESCRIPTION: 10 ft Light Pole Base

MEMBER GEOMETRY DATA	\:		LOAD DATA:		
Pole Height:	10	ft	Pole Weight:	54	lb/ft of height
Pole Diameter:	19	in	Luminaire Weight:	54	lb each
Pedestal Base Height:	6	in	Arm Weight:	100	lb each
Pedestal Base Diameter:	3	ft	Total Weight:	848	lb
Pole Shape:	round - ro	ough			
			SEISMIC FORC	E DATA:	
Number of Arms:	2		Seismic Accel.:	0.287	(ASD - worst case)
Arm Length:	15	in	F _{pole} :	155	lb
Arm Rise:	32	in	F _{luminaires} :	31	lb
Arm Diameter:	6	in	F_{arms} :	57	lb
Luminaire Area:	2.0	sf	E total:	243	lb
Arm + Luminaire Area:	5.3	sf			
Luminaire Shape:	round - ve	ery rough			
T.O. Pole Ht:	10.50	ft			
WIND FORCE DATA:					
Risk Category:	I - All except	I, III, & IV	α:	9.5	
V:	99	mph	z_g :	900	ft
Exposure Category:	С				
K_{zt} :	1.0				
G:	0.85				
			Luminaire		
Pole			z:	13.17	ft
Z:	5.50	ft	K _{z (luminaire)} :	0.85	
K _{z (pole)} :	0.85		K _{d (luminaire)} :	0.95	
K _{d (pole)} :	0.95		q_z :	20.23	psf
q _z :	20.23	psf	A _{f (luminaire)} :	5.25	sf
A _{f (pole)} :	15.83	sf	s/h:	0.16	
h/D:	6.32		B/s:	1.19	
C _{f (pole)} :	0.79		C _{f (luminaire)} :	1.95	
P:	13.56	psf	P:	33.54	psf
F:	215	lb	F:	176	lb
RESULTANT FORCE:			Calamita		
W	(0		Seismic	242	II.
Wind F _{res} :	(Governs)	l b	F _{res} :	243	lb
	391	lb 4	h:	8.28	ft
h:	8.95 3499	ft ft-lb	M(base): V(base):	2016 243	ft-lb
M(base):			v(pase):	∠43	lb
V(base):	391	lb			
ASD F _{res} :	SD WIND = 0.60° 234	<i>₩</i> Ib			
ASD M(base):	2100	ft-lb			
ASD V(base):	234	lb			

NOTES: Delphi Pole

DESCRIPTION: 10 ft Light Pole Base

MEMBER GEOMETRY DATA:

h (ht. of load): 8.95 ft d (embed) (guess): ft b (dia) (guess): 3 ft

LOAD DATA:

AXIAL

P DL: 848 lb P LL: P TL: 100 948 lb

Base Height: 6 in Wt. of Concr.: 150 q_{ALLOW} : 2000 psf

LATERAL

Lateral F: 234 lb

Lateral Bearing: 100 lb/ft²/ft←

Use 2x increase?: (y/n)

Allowable Lateral Bearing: 200 lb/ft²/ft 100 pcf used based on table 1806.2 in the IBC.

NON-CONSTRAINED DESIGN:

d (embed) (guess): 4.00 ft

b (dia): 3.00 ft

d (calc.): 2.95 S1: 267 ft psf Use: 4.00 ft 0.686

CONSTRAINED DESIGN:

4.00 d (embed) (guess):

b (dia): 3.00 ft

d (calc.): 1.93 ft 800 S3: psf

Use: 4.00 ft

CHECK BEARING:

Design Method: Nonconstrained

Footing Area: ft² 7.1

Total Concr. Press.: 75

qBEARING: 209 psf OK

Use:			
d:	4.00	ft	
b:	3	ft	
Vol. Concr.:	31.8	cf	

COMPARISON:

Diameter, b (ft):	3.00	3.25	3.50	3.75	4.00	4.25	4.50
Req'd depth, d (ft):	4.00	4.00	4.00	4.00	4.00	4.00	4.00
Volume of Concrete (cf):	31.8	37.3	43.3	49.7	56.5	63.8	71.6

Caisson Reinforcing Seismic Design Category C, D, E, F $_{\rm IBC \, and \, ACI \, 318}$

Notes: Delphi Pole

Description: 10 ft Light Pole Base

Caisson I	Caisson Dimensions		Longitudinal Reinforcing			
Caisson Diameter:	36 in	Longitudinal Reinf Ratio:	0.005	Bar Size:	4	
Caisson Area:	1018 in ²	Longitudinal As req'd:	5.09 in ²	Spacing:	9 in	
Embedded Pipe Area:	0 in ²	Longitudinal Bar Size:	6			
Net Conc Area:	1018 in ²	No. Bars Req'd:	12			
Perimeter:	113.1 in	Spacing:	10.3 in			
		(reference 18.10.3.9 for min re	einforced Length)			
S:	4580 in ³	SDC:	D			
f'c:	4500 psi					
cracking φ Mn:	69.1 k-ft	Per IBC 18.10.3.9, if design	$Mu > \phi Mn OR if subjection$	ct to uplift,		
Design Mu:	3.5 k-ft	reinforcing as noted above is required in caisson				

NOTES: Huntington Pole

DESCRIPTION: 15 ft Light Pole Base

MEMBER GEOMETRY DATA	A:		LOAD DATA:		
Pole Height:	15	ft	Pole Weight:	73	lb/ft of height
Pole Diameter:	19	in	Luminaire Weight:	54	lb each
Pedestal Base Height:	6	in	Arm Weight:	100	lb each
Pedestal Base Diameter:	3	ft	Total Weight:	1403	lb
Pole Shape:	round - ro	ough			
			SEISMIC FOR	CE DATA:	
Number of Arms:	2		Seismic Accel.:	0.287	(ASD · worst case)
Arm Length:	15	in	F _{pole} :	314	lb
Arm Rise:	32	in	F _{luminaires} :	31	lb
Arm Diameter:	6	in	F _{arms} :	57	lb
Luminaire Area:	2.0	sf	E total:	403	lb
Arm + Luminaire Area:	5.3	sf			
Luminaire Shape:	round - ve	ery rough			
T.O. Pole Ht:	15.50	ft			
WIND FORCE DATA:					
Risk Category:	II - All except	: I, III, & IV	α:	9.5	
V:	99	mph	Z _q :	900	ft
Exposure Category:	С	·	9		
K _{zt} :	1.0				
G:	0.85				
			Luminaire		
Pole			z:	18.17	ft
Z:	8.00	ft	K _{z (luminaire)} :	0.88	
K _{z (pole)} :	0.85		K _{d (luminaire)} :	0.95	
K _{d (pole)} :	0.95		q _z :	21.07	psf
q _z :	20.23	psf	A _{f (luminaire)} :	5.25	sf
A _{f (pole)} :	23.75	sf	s/h:	0.12	
h/D:	9.47		B/s:	1.19	
C _{f (pole)} :	0.81		C _{f (luminaire)} :	1.95	
P:	14.00	psf	P:	34.92	psf
F:	332	lb	F:	183	lb
RESULTANT FORCE:					
			Seismic	(Governs)	
Wind			F_{res} :	403	lb
F _{res} :	516	lb	h:	10.23	ft
h:	11.61	ft	M(base):	4120	ft-lb
M(base):	5989	ft-lb	V(base):	403	lb
V(base):	516	lb			
	ASD WIND = 0.60	*W			
ASD F _{res} :	309	lb			
ASD M(base):	3594	ft-lb			
ASD V(base):	309	lb			

NOTES: Huntington Pole

DESCRIPTION: 15 ft Light Pole Base

MEMBER GEOMETRY DATA:

h (ht. of load): 10.23 ft d (embed) (guess): 4 ft b (dia) (guess): 3 ft

LOAD DATA:

AXIAL

P DL: 1403 | Ib P LL: 100 | Ib | P TL: 1503

 $\begin{array}{cccc} \text{Base Height:} & \text{6} & \text{in} \\ \text{Wt. of Concr.:} & 150 & \text{pcf} \\ & \text{q}_{\text{ALLOW}} : & 2000 & \text{psf} \end{array}$

LATERAL

Lateral F: 403 lb

Lateral Bearing: 100 lb/ft²/ft< Use 2x increase?: Y (y/n)

Allowable Lateral Bearing: 200 lb/ft²/ft

100 pcf used based on table 1806.2 in the IBC.

lb

NON-CONSTRAINED DESIGN:

d (embed) (guess): 4.25 ft

b (dia): 3.00 ft

d (calc.): 4.11 ft S1: 283 psf
Use: 4.25 ft A: 1.109

CONSTRAINED DESIGN:

d (embed) (guess): 4.25 ft

b (dia): 3.00 ft

d (calc.): 2.62 ft S3: 850 psf

Use: 4.25 ft

CHECK BEARING:

Design Method: Nonconstrained

Footing Area: 7.1 ft²

Total Concr. Press.: 75 psf

q_{BEARING}: 288 psf OK

Use:

d: 4.25 ft

b: 3 ft

Vol. Concr.: 33.6 cf

COMPARISON:

Diameter, b (ft):	3.00	3.25	3.50	3.75	4.00	4.25	4.50
Req'd depth, d (ft):	4.25	4.25	4.00	4.00	4.00	4.00	4.00
Volume of Concrete (cf):	33.6	39.4	43.3	49.7	56.5	63.8	71.6

Caisson Reinforcing Seismic Design Category C, D, E, F $_{\rm IBC \, and \, ACI \, 318}$

Notes: Huntington Pole Description: 15 ft Light Pole Base

Caisson I	Dimensions	Longitudinal Reinfo	Longitudinal Reinforcing		e Reinforcing		
Caisson Diameter:	36 in	Longitudinal Reinf Ratio:	0.005	Bar Size:	4		
Caisson Area:	1018 in ²	Longitudinal As req'd:	5.09 in ²	Spacing:	9 in		
Embedded Pipe Area:	0 in ²	Longitudinal Bar Size:	6				
Net Conc Area:	1018 in ²	No. Bars Req'd:	12				
Perimeter:	113.1 in	Spacing:	10.3 in				
		(reference 18.10.3.9 for min re	einforced Length)				
S:	4580 in ³	SDC:	D				
f'c:	4500 psi						
cracking φ Mn:	69.1 k-ft	Per IBC 18.10.3.9, if design	$Mu > \phi Mn OR if subject$	t to uplift,			
Design Mu:	6.0 k-ft	reinforcing as noted above is required in caisson					

Notes: Fremont Pole

DESCRIPTION: 14.5 ft Light Pole Base

MEMBER GEOMETRY DATA	N:		LOAD DATA:		
Pole Height:	14.5	ft	Pole Weight:	36	lb/ft of height
Pole Diameter:	14	in	Luminaire Weight:	55	lb each
Pedestal Base Height:	6	in	Arm Weight:	150	lb each
Pedestal Base Diameter:	3	ft	Total Weight:	932	lb
Pole Shape:	round - ro	ough			
			SEISMIC FORC	E DATA:	
Number of Arms:	2		Seismic Accel.:	0.287	(ASD - worst case)
Arm Length:	48	in	F _{pole} :	150	lb
Arm Rise:	52	in	F _{luminaires} :	32	lb
Arm Diameter:	7	in	F _{arms} :	86	lb
Luminaire Area:	3.5	sf	E total:	267	lb
Arm + Luminaire Area:	11.7	sf			
Luminaire Shape:	round - ve	ery rough			
T.O. Pole Ht:	15.00	ft			
WIND FORCE DATA:					
Risk Category:	II - All except	t I, III, & IV	α:	9.5	
V:	99	mph	Z _g :	900	ft
Exposure Category:	С		•		
K _{zt} :	1.0				
G:	0.85				
			Luminaire		
Pole			Z:	19.33	ft
z:	7.75	ft	K _{z (luminaire)} :	0.90	
K _{z (pole)} :	0.85		K _{d (luminaire)} :	0.95	
K _{d (pole)} :	0.95		q _z :	21.34	psf
q _z :	20.23	psf	A _{f (luminaire)} :	11.67	sf
A _{f (pole)} :	16.92	sf	s/h:	0.08	
h/D:	12.43		B/s:	5.49	
C _{f (pole)} :	0.83		C _{f (luminaire)} :	1.95	
P:	14.28	psf	P:	35.38	psf
F:	242	lb	F:	413	lb
RESULTANT FORCE:					
			Seismic		
Wind	(Governs)		F _{res} :	267	lb
F _{res} :			la .	10 05	£1
	654	lb	h:	12.85	ft
h:	15.06	lb ft	M(base):	3436	ft-lb
M(base):	15.06 9852				
	15.06	ft	M(base):	3436	ft-lb
M(base): V(base):	15.06 9852 654 ASD WIND = 0.60	ft ft-lb lb *W	M(base):	3436	ft-lb
M(base): V(base): ASD F _{res} :	15.06 9852 654 SD WIND = 0.60	ft ft-lb lb *W lb	M(base):	3436	ft-lb
M(base): V(base):	15.06 9852 654 ASD WIND = 0.60	ft ft-lb lb *W	M(base):	3436	ft-lb

NOTES: Fremont Pole

DESCRIPTION: 14.5 ft Light Pole Base

MEMBER GEOMETRY DATA:

h (ht. of load): 15.06 ft d (embed) (guess): 3 ft 3 b (dia) (guess): ft

LOAD DATA:

AXIAL

P DL: 932 lb P LL: P TL: 100 1032 lb

Base Height: 6 in Wt. of Concr.: 150 q_{ALLOW} : 2000 psf

LATERAL

Lateral F: 393 lb

Lateral Bearing: 100 lb/ft²/ft←

Use 2x increase?: (y/n)

Allowable Lateral Bearing: 200 lb/ft²/ft 100 pcf used based on table 1806.2 in the IBC.

NON-CONSTRAINED DESIGN:

d (embed) (guess): 4.75 ft

b (dia): 3.00 ft

d (calc.): 4.50 S1: 317 ft psf Use: 4.75 ft 0.967

CONSTRAINED DESIGN:

d (embed) (guess): 4.75 3.00 b (dia): ft

d (calc.): 2.97 ft 950 S3: psf

Use: 4.75 ft

CHECK BEARING:

Design Method: Nonconstrained

Footing Area: ft² 7.1 Total Concr. Press.:

75 **q**BEARING: 221 psf OK

Use: 4.75 3 ft Vol. Concr.: 37.1

COMPARISON:

Diameter, b (ft):	3.00	3.25	3.50	3.75	4.00	4.25	4.50
Req'd depth, d (ft):	4.75	4.50	4.50	4.25	4.25	4.25	4.00
Volume of Concrete (cf):	37.1	41.5	48.1	52.5	59.7	67.4	71.6

Caisson Reinforcing Seismic Design Category C, D, E, F

IBC and ACI 318

Notes: Fremont Pole

Description: 14.5 ft Light Pole Base

Caisson Dimensions		Longitudinal Reinfo	Transverse Reinforcing			
Caisson Diameter:	36 in	Longitudinal Reinf Ratio:	0.005	Bar Size:	4	
Caisson Area:	1018 in ²	Longitudinal As req'd:	5.09 in ²	Spacing:	9 in	
Embedded Pipe Area:	0 in ²	Longitudinal Bar Size:	6			
Net Conc Area:	1018 in ²	No. Bars Req'd:	12			
Perimeter:	113.1 in	Spacing:	10.3 in			
		(reference 18.10.3.9 for min re	einforced Length)			
S:	4580 in ³	SDC:	D			
f'c:	4500 psi					
cracking φ Mn:	69.1 k-ft	Per IBC 18.10.3.9, if design	$Mu > \phi$ Mn OR if subjec	t to uplift,		
Design Mu:	9.9 k-ft	reinforcing as noted above is required in caisson				